## **REGULAR ARTICLE**

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# On the accuracy of numerical Hartree–Fock energies

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**Abstract** It is demonstrated that numerical Hartree–Fock (HF) energies reported in the literature in some cases have errors in the milliHartree range. The main cause of these errors is due to the use of too small a value for the 'practical infinity' parameter in the finite difference method for generating the results. By systematically investigating the convergence with respect to the computational parameters, HF energies accurate to at least 1 microHartree are generated for 42 diatomic systems containing first and second row elements, encompassing both cationic, neutral and anionic systems.

## **1** Introduction

The prediction of molecular stabilities by first-principle electronic structure methods is a subject that has attracted much attention over the last decade. The theoretical framework is conceptually simple: determine the minimum energy geometry, estimate the infinite-correlation infinite-basis-set limit for the electronic energy, and add vibrational zero-point energies and finite temperature corrections to give molecular heat of formation, which can be directly related to experimental results. A brute force approach for the second step, estimating the infinite-correlation infinite-basis-set limit, is not feasible, and composite methods are often used instead, as exemplified by the CBS-n [1], Gn [2], Wn [3] and focal point [4] methods. The computationally difficult part in these methods is estimating the correlation energy, but extrapolations [5] based on the correlation-consistent basis sets [6] or the use of explicitly correlated wave functions [7] have made a large step towards solving this problem. The basis set convergence of the Hartree-Fock (HF) energy is significantly faster than the correlation energy, and the HF basis set error is often assumed to be negligible, but as the effort towards higher accuracy continues, this error at some point must also be addressed.

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For atoms and diatomic systems, the limiting HF energy can be obtained by solving the integro-differential equations by finite difference or finite elements methods [8], and these results provide an absolute reference against which the results from finite basis sets can be evaluated. We have recently proposed a hierarchy of polarization-consistent basis sets [9, 10], which, although optimized for density functional methods, should also be suitable for estimating the HF basis set limit. In connection with this work, we have in several cases obtained energies by (large) basis set calculations that were significantly different or even lower than the limiting HF energies reported in the literature, casting doubt on the accuracy of these results. In the present paper, we examine the cause of these discrepancies, and report HF energies for a selection of diatomic systems composed of first and second row elements, which should be accurate to at least 1 microHartree.

### 2 Results and discussion

All calculations have been done using the 2dhf program [11], which solves the integro-differential HF equations by a finite difference method [8]. The orbital densities are evaluated on a grid in the transformed prolate spheroidal coordinates vand  $\mu$  used for representing the radial wave function, while the angular part is solved analytically. The method in addition employs a 'practical infinity' distance parameter  $(R_{\infty})$ for estimating the asymptotic behavior in the  $\mu$  coordinate. The accuracy of a finite difference HF calculation is thus determined by four parameters: the grid sizes for the  $\nu$  and  $\mu$ coordinates, the value for  $R_{\infty}$  and the convergence criteria for terminating the iterative procedure. If the increment between grid points in the  $\nu$  and  $\mu$  coordinates is chosen to be equal, the number of independent parameters is reduced to three, and this has been employed in the present case. A constant grid spacing determined by the number of  $\nu$  grid points has as the consequence that the number of  $\mu$  grid points increases with  $R_{\infty}$ , as reflected in Tables 1, 2 and 3. The convergence criterion has in all cases been set to  $10^{-12}$ , which is sufficient

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| System                       | Grid                                 | $R_{\infty}$ | HF energy  |
|------------------------------|--------------------------------------|--------------|--|
| $^{1}CH^{+}$                 | 169×193                              | 30           | -37.9099113 <sup>a</sup>                         |
| R = 2.137 au                 | $169 \times 229$                     | 40           | -37.9099112                                      |
|                              | 175×325                              | 200          | -37.9099112                                      |
| _                            | $217 \times 403$                     | 200          | -37.9099112                                      |
| <sup>3</sup> CH <sup>-</sup> | 169×229                              | 40           | -38.2933200                                      |
| $R = 2.20  \mathrm{au}$      | 175×325                              | 200          | -38.2933200                                      |
|                              | 217×403                              | 200          | -38.2933200                                      |
| <sup>3</sup> NH              | 81×105                               |              | -54.978429 <sup>b</sup>                          |
| R = 1.9614 au                | 169×235                              | 40           | -54.9784239                                      |
|                              | 175×331                              | 200          | -54.9784239                                      |
|                              | $217 \times 409$                     | 200          | -54.9784239                                      |
| $^{1}OH^{-}$                 | $211 \times 211$                     | 45           | $-75.4188033^{a}$                                |
| R = 1.781 au                 | $169 \times 241$                     | 40           | -75.4188031                                      |
|                              | $175 \times 337$                     | 200          | -754188031                                       |
|                              | $217 \times 415$                     | 200          | -754188031                                       |
| <sup>1</sup> FH              | 81×161                               | 200          | $-100.07082^{\circ}$                             |
| R = 1.7328 au                | $160 \times 103$                     | 30           | -100.07082<br>$-100.0708028^{3}$                 |
| K = 1.7526  au               | 160, 252                             | 50           | -100.0708028                                     |
|                              | 169×255                              | 60<br>40     | $-100.0708025^{\circ}$                           |
|                              | 169×241                              | 40           | -100.0708025                                     |
|                              | 1/5×33/                              | 200          | -100.0708025                                     |
| 1~                           | 217×421                              | 200          | -100.0708025                                     |
| $^{1}C_{2}$                  |                                      |              | $-75.406565^{e}$                                 |
| R = 2.358 au                 | $169 \times 223$                     | 40           | -75.4065652                                      |
|                              | 175×319                              | 200          | -75.4065652                                      |
|                              | 217×397                              | 200          | -75.4065652                                      |
| <sup>2</sup> CN              | 319×415                              | 40           | $-92.2251341^{f}$                                |
| R = 1.1718  Å                | 169×229                              | 40           | -92.2251382                                      |
|                              | 175×325                              | 200          | -92.2251382                                      |
|                              | 217×403                              | 200          | -92.2251382                                      |
| $^{1}CN^{-}$                 | $211 \times 211$                     | 50           | -92.3489506 <sup>a</sup>                         |
| R = 2.214 au                 | $169 \times 229$                     | 40           | -92.3489505                                      |
|                              | $175 \times 325$                     | 200          | -92.3489505                                      |
|                              | $217 \times 403$                     | 200          | -92 3489506                                      |
| <sup>1</sup> N <sub>2</sub>  | $57 \times 105$                      | 200          | -108 993810                                      |
| R = 2.068  au                | $270 \times 220$                     | 25           | -108.00382578                                    |
| h = 2.000  au                | $160 \times 103$                     | 20           | $-108.9938237^{\circ}$<br>$-108.0038260^{\circ}$ |
|                              | 160 × 220                            | 40           | -108.9938200                                     |
|                              | 109 × 229                            | 200          | -108.9938230                                     |
|                              | $173 \times 323$<br>$217 \times 400$ | 200          | -108.9938230                                     |
| INO+                         | 21/X409                              | 200          | -100.9956250                                     |
| 'NU'                         | 169×193                              | 30<br>40     | -128.9780510                                     |
| R = 2.007 au                 | 169×235                              | 40           | -128.9780515                                     |
|                              | 1/5×331                              | 200          | -128.9780515                                     |
| 1                            | 217×409                              | 200          | -128.9780515                                     |
| <sup>1</sup> NO <sup>-</sup> | $169 \times 223$                     | 40           | -129.2801373                                     |
| $R = 2.36  \mathrm{au}$      | 175×319                              | 200          | -129.2801743                                     |
|                              | 175×331                              | 250          | -129.2801744                                     |
|                              | 175×343                              | 300          | -129.2801745                                     |
|                              | 217×427                              | 300          | -129.2801745                                     |
| <sup>1</sup> CO              | 81×113                               |              | -112.79095°                                      |
| R = 2.132 au                 | 169×193                              | 25           | -112.790906 <sup>g</sup>                         |
|                              | 169×253                              | 60           | $-112.7909072^{d}$                               |
|                              | 169×229                              | 40           | -112.7909072                                     |
|                              | $175 \times 325$                     | 200          | -112.7909072                                     |
|                              | 217, 402                             | 200          | 112 7000072                                      |

**Table 1** Convergence of the HF energy as a function of the grid size and  $R_{\infty}$  parameter for systems composed of first row elements. Grid is the number of grid points in the v and  $\mu$  coordinates, respectively

Table 1 (Contd.)

| System                                 | Grid                                 | $R_{\infty}$ | HF energy                    |
|--|--------------------------------------|--------------|------------------------------|
| <sup>3</sup> O <sub>2</sub>            | 169×277                              | 90           | $-149.6687531^{d}$           |
| R = 2.270 au                           | 169×223                              | 40           | -149.6687096                 |
|  | 175×325                              | 200          | -149.6687569                 |
|  | 175×337                              | 250          | -149.6687571                 |
|  | 175×343                              | 300          | -149.6687572                 |
|  | 217×427                              | 300          | -149.6687572                 |
| $^{1}CF^{+}$                           | 169×193                              | 30           | $-136.9001351^{a}$           |
| R = 2.322 au                           | 169×223                              | 40           | -136.9001348                 |
|  | 175×319                              | 200          | -136.9001348                 |
|  | 217×397                              | 200          | -136.9001348                 |
| <sup>3</sup> CF <sup>-</sup>           | 169×217                              | 40           | -137.2244623                 |
| $R = 2.78  \mathrm{au}$                | 175×313                              | 200          | -137.2244560                 |
|  | 175×343                              | 350          | -137.2244562                 |
|  | 217×427                              | 350          | -137.2244562                 |
| <sup>3</sup> NF                        | $169 \times 253$                     | 60           | $-153.8424180^{d}$           |
| $R = 2.49 \mathrm{au}$                 | $169 \times 223$                     | 40           | -1538424147                  |
| n – 2.17 uu                            | $175 \times 319$                     | 200          | -153.8424211                 |
|  | $175 \times 343$                     | 300          | -153.8424212                 |
|  | $217 \times 397$                     | 300          | -153.8424212                 |
| $^{1}OF^{-}$                           | $169 \times 211$                     | 40           | -174 2362661                 |
| $R = 2.82 \mathrm{au}$                 | $105 \times 211$<br>$175 \times 313$ | 200          | -174.2362001                 |
| $n = 2.02  \mathrm{du}$                | $175 \times 331$                     | 300          | -174.2363415                 |
|  | $175 \times 343$                     | 350          | -1742363416                  |
|  | $217 \times 427$                     | 350          | -1742363416                  |
| <sup>1</sup> Fa                        | 21//(12/                             | 550          | $-198773323^{\circ}$         |
| R = 2.668  au                          | $247 \times 439$                     | 160          | _198 7734430d                |
| K = 2.000  au                          | $160 \times 103$                     | 30           | $-198.7724238^{a}$           |
|  | $169 \times 217$                     | 40           | _198 7733129                 |
|  | $109 \times 217$<br>$175 \times 313$ | 200          | -198.773/129<br>-108.773/130 |
|  | $175 \times 315$<br>$175 \times 337$ | 200          | -198.7734439<br>-108.7734446 |
|  | $175 \times 337$<br>$175 \times 343$ | 350          | -198.7734440<br>-108.7734447 |
|  | $173 \times 343$<br>$217 \times 427$ | 350          | -198.7734447<br>-108.7734448 |
| 2 <b>E</b> -                           | $160 \times 205$                     | 40           | 108 8621270                  |
| $\frac{\Gamma_2}{R} = 2.52 \text{ cm}$ | $109 \times 203$<br>$175 \times 201$ | 200          | -198.8021279                 |
| K = 5.52  au                           | $175 \times 301$<br>$175 \times 331$ | 200          | -198.8023397                 |
|  | 175×331                              | 400          | -198.8023012                 |
|  | $1/3 \times 33/$                     | 400          | -198.8023013                 |
|  | $217 \times 421$<br>$250 \times 400$ | 400          | -198.8023013                 |
|  | 239 × 499                            | 400          | -198.8023013                 |
| <sup>a</sup> Ref. [12]                 |                                      |              |                              |
| <sup>b</sup> Ref. [13]                 |                                      |              |                              |
| <sup>c</sup> Ref. [14]                 |                                      |              |                              |
| <sup>a</sup> Ref. [9]                  |                                      |              |                              |
| <sup>e</sup> Ref. [15]                 |                                      |              |                              |
| <sup>1</sup> Ref. [16]                 |                                      |              |                              |
| <sup>g</sup> Ref. [17]                 |                                      |              |                              |

function of the  $\nu$  grid size and the  $R_{\infty}$  parameter, and the last entry in each case should be within ~0.2 microHartree of the limiting value. It should be noted that the energy does not vary monotonic with the  $R_{\infty}$  parameter. As a check of the accuracy of the final results, we have also estimated the HF limit by extrapolation of the results using the aug-pc-2, -3 and -4 basis sets, and these energies in each case agree with the numerical results to with a few tenths of a microHartree.

For the first row systems in Table 1, it is clear that a typical  $R_{\infty}$  value of 40 au is sufficient for species like C<sub>2</sub> and N<sub>2</sub>, but inadequate for system like O<sub>2</sub> and F<sub>2</sub>, where a cutoff value of ~300 au is required for converging the results to a microHartree accuracy. We note that several literature values deviate by several tenths of a microHartree relative to the converged results. Furthermore, the employed  $R_{\infty}$  value

to ensure convergence to at least  $\sim 0.02$  microHartree for the present systems.

Tables 1, 2 and 3 list HF energies for 42 diatomic species composed of first and second row elements having wave functions of  $\sum$  symmetry. The total energy is given as a

**Table 2** Convergence of the HF energy as a function of the grid size and  $R_{\infty}$  parameter for systems composed of first and second row elements. Grid is the number of grid points in the  $\nu$  and  $\mu$  coordinates, respectively

| Table 2 | (Contd.) |
|---------|----------|
|---------|----------|

| System                        | Grid                                 | $R_\infty$ | HF energy                 |
|-------------------------------|--------------------------------------|------------|---------------------------|
| <sup>3</sup> SiH <sup>-</sup> | 169×211                              | 40         | -289.4646220              |
| R = 2.94 au                   | 175×307                              | 200        | -289.4646297              |
|                               | 175×331                              | 300        | -289.4646298              |
|                               | $217 \times 409$                     | 300        | -289.4646301              |
|                               | 259×493                              | 300        | -289.4646301              |
| <sup>1</sup> SH <sup>-</sup>  | 211×211                              | 50         | -398.1497921ª             |
| R = 2.551 au                  | 169×217                              | 40         | -398.1497798              |
|                               | 175×319                              | 200        | -398.1497904              |
|                               | 175×337                              | 300        | -398.1497904              |
|                               | 217×421                              | 300        | -398.1497908              |
|                               | 259×505                              | 300        | -398.1497909              |
| <sup>1</sup> HCl              | 169×223                              | 40         | -460.1124388              |
| R = 2.44 au                   | 175×319                              | 200        | -460.1124488              |
|                               | 175×343                              | 300        | -460.1124489              |
|                               | 217×427                              | 300        | -460.1124493              |
|                               | $259 \times 505$                     | 300        | -460.1124493              |
| $^{2}CP$                      | $169 \times 211$                     | 40         | -378 4745976              |
| R = 3.08  au                  | $175 \times 307$                     | 200        | -378 4746077              |
| R = 5.00 dd                   | $175 \times 331$                     | 300        | -3784746078               |
|                               | $217 \times 409$                     | 300        | -378 4746084              |
|                               | $259 \times 487$                     | 300        | -378.4746084              |
| <sup>1</sup> CP <sup>-</sup>  | $169 \times 211$                     | 40         | -378 5615775              |
| R = 3.00  au                  | $105 \times 211$<br>$175 \times 307$ | 200        | -378 5615880              |
| K = 5.00 dd                   | $175 \times 331$                     | 300        | -378 5615881              |
|                               | $217 \times 409$                     | 300        | -378 5615886              |
|                               | $259 \times 493$                     | 300        | -3785615887               |
| <sup>1</sup> CS               | $121 \times 121$                     | 200        | $-435.36273^{b,c}$        |
| R = 2.89964 au                | 193×229                              | 40         | -435 3624198 <sup>d</sup> |
| R = 2.0000 au                 | $169 \times 211$                     | 40         | -435 3624291              |
|                               | $175 \times 307$                     | 200        | -4353624195               |
|                               | $175 \times 331$                     | 300        | -435 3624195              |
|                               | $217 \times 415$                     | 300        | -435 3624202              |
|                               | $259 \times 493$                     | 300        | -435.3624203              |
| <sup>2</sup> SiN              | $121 \times 137$                     | 30         | -343 353489e              |
| R = 1.575Å                    | $169 \times 211$                     | 40         | -343 2970349              |
| R = 1.575R                    | $105 \times 211$<br>$175 \times 307$ | 200        | -343 2970265              |
|                               | $175 \times 331$                     | 300        | -343 2970265              |
|                               | $217 \times 409$                     | 300        | -3432970203               |
|                               | $259 \times 493$                     | 300        | -343 2970269              |
| 1SIN-                         | $160 \times 211$                     | 40         | -343 3623740              |
| R = 2.94 au                   | $109 \times 211$<br>$175 \times 307$ | 200        | -343 3623652              |
|                               | $175 \times 307$<br>$175 \times 331$ | 300        | -3433623652               |
|                               | $175 \times 551$<br>$217 \times 400$ | 300        | -343.3623652              |
|                               | $217 \times 409$<br>$259 \times 493$ | 300        | -343 3623656              |
| <sup>1</sup> NP               | $121 \times 121$                     | 500        | _305 1886/b               |
| R = 2.8173  au                | $121 \times 121$<br>$160 \times 211$ | 40         | -395.1884040              |
| n = 2.01/3 au                 | 175~313                              | 200        | -395.1883050              |
|                               | 175~313                              | 200        | -395.18830/0              |
|                               | $217 \times 415$                     | 300        | -305 1883053              |
|                               | 250~103                              | 300        | _305 1883054              |
|                               | 2J7X493                              | 500        | -373.1003934              |

| ${}^{3}\text{SN}^{-}$ $R = 3.12 \text{ au}$ $169 \times 211$ $40$ $-451.$ $R = 3.12 \text{ au}$ $175 \times 307$ $200$ $-451.$ $175 \times 325$ $300$ $-451.$ $217 \times 415$ $350$ $-451.$ $259 \times 499$ $350$ $-451.$ $259 \times 499$ $350$ $-451.$ $R = 3.14 \text{ au}$ $175 \times 307$ $200$ $-513.$ $175 \times 325$ $300$ $-513.$ | 9875815<br>9876478<br>9876482<br>9876482<br>9876492<br>9876493<br>9069810<br>9070118<br>9070118<br>9070113<br>9070133<br>9070135<br>85548 <sup>b</sup><br>855348 <sup>b</sup> |
|--|---|
| $R = 3.12$ au $175 \times 307$ $200$ $-451.$ $175 \times 325$ $300$ $-451.$ $175 \times 337$ $350$ $-451.$ $217 \times 415$ $350$ $-451.$ $259 \times 499$ $350$ $-451.$ $3$ NCl $169 \times 211$ $40$ $-513.$ $R = 3.14$ au $175 \times 307$ $200$ $-513.$ $175 \times 325$ $300$ $-513.$   | 9876478<br>9876481<br>9876482<br>9876492<br>9876493<br>9069810<br>9070118<br>9070118<br>90701135<br>85548 <sup>b</sup><br>855348 <sup>b</sup><br>8553486                      |
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| $ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$  | 9876482<br>9876492<br>9876493<br>9069810<br>9070118<br>9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>855348 <sup>b</sup><br>8553485                                  |
| $\begin{array}{cccccccc} & & 217 \times 415 & 350 & -451. \\ & & 259 \times 499 & 350 & -451. \\ 3^{3}\text{NCl} & & 169 \times 211 & 40 & -513. \\ R = 3.14 \text{ au} & & 175 \times 307 & 200 & -513. \\ & & 175 \times 325 & 300 & -513. \end{array}$  | 9876492<br>9876493<br>9069810<br>9070118<br>9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>855348 <sup>b</sup><br>8553485   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 9876493<br>9069810<br>9070118<br>9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>855348 <sup>b</sup><br>8553486<br>8553415   |
| <sup>3</sup> NCl $169 \times 211$ 40 $-513.$<br>$R = 3.14$ au $175 \times 307$ 200 $-513.$<br>$175 \times 325$ 300 $-513.$   | 9069810<br>9070118<br>9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>8553486<br>8553415   |
| $\begin{array}{cccc} R = 3.14  \mathrm{au} & 175 \times 307 & 200 & -513. \\ 175 \times 325 & 300 & -513. \end{array}$   | 9070118<br>9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>8553486<br>8553415  |
| $175 \times 325$ 300 $-513$ .  | 9070118<br>9070133<br>9070135<br>85548 <sup>b</sup><br>8553486<br>8553415   |
|  | 9070133<br>9070135<br>85548 <sup>b</sup><br>8553486<br>8553415  |
| $217 \times 409$ 300 -513.   | 9070135<br>85548 <sup>b</sup><br>8553486<br>8553415   |
| 259×487 300 -513.  | 85548°<br>8553486<br>8553415  |
| $^{1}SiO$ 121×121 $-363$ .   | 8553486<br>8553415  |
| $R = 2.853 \mathrm{au}$ 169×211 40 -363.   | 8553415   |
| $175 \times 313$ 200 $-363$ .  | 0000710   |
| $175 \times 331$ $300$ $-363$ .  | 8553414   |
| $217 \times 415$ 300 $-363$ .  | 8553418   |
| $259 \times 493$ 300 $-363$ .  | 8553418   |
| $^{3}PO^{-}$ 169×211 40 -415.  | 6564135   |
| $R = 2.90 \mathrm{au}$ 175×307 200 -415.   | 6564649   |
| $175 \times 319$ 250 -415.   | 6564651   |
| $175 \times 331$ 300 -415.   | 6564652   |
| $217 \times 415$ 300 -415.   | 6564657   |
| $259 \times 493$ 300 -415.   | 6564658   |
| $^{3}SO$ 169×211 40 -472.  | 3990425   |
| $R = 2.87 \mathrm{au}$ 175×307 200 -472.   | 3991036   |
| $175 \times 331$ 300 -472.   | 3991039   |
| $175 \times 343$ 350 -472.   | 3991040   |
| $217 \times 421$ 350 -472.   | 3991047   |
| $259 \times 505$ 350 -472.   | 3991048   |
| $^{1}\text{SF}^{-}$ 169×205 40 -497.   | 0283170   |
| R = 3.22  au 175×301 200 -497.   | 0283455   |
| $175 \times 313$ 250 $-497$ .  | 0283456   |
| $175 \times 325$ 300 $-497$ .  | 0283457   |
| $217 \times 403$ 300 $-497$ .  | 0283469   |
| $259 \times 487$ 300 $-497$ .  | 0283470   |
| $^{3}\text{PF}$ 169×211 40 -440.   | 2339052   |
| $R = 3.015 \mathrm{au}$ 175×307 200 -440.  | 2339244   |
| $175 \times 331$ 300 -440.   | 2339245   |
| $217 \times 409$ 300 -440.   | 2339251   |
| $259 \times 487$ 300 -440.   | 2339252   |
| $^{1}\text{CIF}$ 169×211 40 -558.  | 9175082   |
| $R = 3.14 \mathrm{au}$ 175×307 200 -558.   | 9176239   |
| $175 \times 325$ 300 $-558$ .  | 9176245   |
| $175 \times 337$ 350 $-558$ .  | 9176247   |
| $175 \times 343$ 400 $-558$ .  | 9176247   |
| 217×415 350 -558.  | 9176261   |
| 259×499 350 -558.  | 017(0/2   |

<sup>a</sup>Ref. [12]

<sup>b</sup>Ref. [18]

 $^{c}R = 2.9006$  au. The corresponding converged value at this geometry is -435.3623913

<sup>d</sup>Ref. [19] <sup>e</sup>Ref. [20]

and convergence criterion for terminating the iterative procedure is often not given, making it difficult to reproduce the reported values. For systems involving second row elements (Tables 2 and 3), the cutoff value must in some cases be even larger, and a significantly larger grid is also required in order to converge the results to within 1 microHartree. For some of the systems (SiN and  $P_2$ ), the converged results deviate from the literature value by several milliHartrees. A priori, it might have been expected that anions with loosely bound electrons would require larger values for  $R_{\infty}$ in order to obtain converged results. The results in Tables 1, 2 and 3, however, only show a weakly trend in this direction. The  $R_{\infty}$  value required for systems like F<sub>2</sub> and Cl<sub>2</sub> is already so large that it also suffices for the corresponding anion. Cations are not expected to have requirements different from the neutral species, and only a few have been included for comparison with literature values.

| System                       | Grid                                 | $R_{\infty}$ | HF energy                |
|------------------------------|--------------------------------------|--------------|--------------------------|
| <sup>1</sup> SiS             | 121×137                              | 30           | -686.516707 <sup>a</sup> |
| $R = 1.93 \text{\AA}$        | 169×199                              | 40           | -686.5162620             |
|                              | 175×295                              | 200          | -686.5162806             |
|                              | $175 \times 307$                     | 250          | -686.5162807             |
|                              | 175×319                              | 300          | -686.5162808             |
|                              | 259×475                              | 300          | -686.5162842             |
|                              | $277 \times 505$                     | 300          | -686.5162842             |
| $^{1}P_{2}$                  | 61×61                                |              | $-681.508^{b}$           |
| R = 3.578 au                 | 169×199                              | 40           | -681.5000151             |
|                              | $175 \times 295$                     | 200          | -681.5002505             |
|                              | 175×331                              | 350          | -681.5002523             |
|                              | $175 \times 337$                     | 400          | -681.5002523             |
|                              | $259 \times 499$                     | 400          | -681.5002552             |
|                              | 295×571                              | 400          | -681.5002553             |
| <sup>3</sup> PS <sup>-</sup> | 169×199                              | 40           | -738.3396168             |
| $R = 3.80  \mathrm{au}$      | $175 \times 295$                     | 200          | -738.3397021             |
|                              | 175×319                              | 300          | -738.3397027             |
|                              | $175 \times 325$                     | 350          | -738.3397026             |
|                              | 259×481                              | 350          | -738.3397073             |
| 2                            | 295×553                              | 350          | -738.3397074             |
| $^{3}S_{2}$                  | 169×199                              | 40           | -795.0911928             |
| $R = 3.642  \mathrm{au}$     | $175 \times 295$                     | 200          | -795.0915518             |
|                              | 175×319                              | 300          | -795.0915540             |
|                              | 175×325                              | 350          | -795.0915541             |
|                              | 259×481                              | 350          | - /95.0915589            |
| 10.01-                       | 295×553                              | 350          | -/95.0915590             |
| 'SCI                         | 169×193                              | 40           | -857.1042706             |
| R = 4.06  au                 | 175×289                              | 200          | -857.1044078             |
|                              | 1/5×331<br>175 - 227                 | 400          | -857.1044093             |
|                              | 1/5×33/<br>250×497                   | 450          | -857.1044093             |
|                              | 259×487<br>205×550                   | 400          | -857.1044184             |
| 101                          | 293 × 339                            | 400          | -037.1044100             |
| $Cl_2$                       | 109×199                              | 40           | -919.0083033             |
| $K = 5.80 \mathrm{au}$       | 1/3×295                              | 200          | -919.0089219             |
|                              | 175×323                              | 400          | -919.0089234             |
|                              | $1/3 \times 331$<br>$250 \times 403$ | 400          | -919.0089233             |
|                              | 239×493                              | 400          | -919.0089343             |
| 101-                         | $293 \times 303$<br>160 × 181        | 400          | -919.0089343             |
| $R_{-}^{12}$ 5 00 au         | 109×101<br>175×277                   | 200          | -919.0783403             |
| $R = 5.00  \mathrm{au}$      | $1/3 \times 2/7$<br>$175 \times 210$ | 200          | -919.0793182             |
|                              | $175 \times 319$<br>$175 \times 325$ | 400          | -919.0793280             |
|                              | $173 \times 323$<br>$250 \times 460$ | 400          | -919.0795279             |
|                              | $239 \times 409$<br>$277 \times 505$ | 400          | -919.0793031             |
|                              | 205 × 535                            | 400          | -919.0795055             |
|                              | 275 × 355                            | 400          | -919.0793037             |
| <sup>a</sup> Ref. [20]       |                                      |              |                          |

<sup>b</sup>Ref. [18]

### **3** Summary

Numerical Hartree–Fock energies with an accuracy of at least  $1 \mu$  Hartree are reported for 42 diatomic species composed of first and second row elements. It is shown that literature values in some cases are in error by several microHartrees for first row systems and by several milliHartrees for second row systems.

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